

# Ice-Accretion Test Results for Three-Large-Scale Swept-Wing Models in the NASA Icing Research Tunnel

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### **Outline**

- Introduction
- Objective and Approach
- Hybrid Model Design
- **Experimental Methodology**
- **Aerodynamic Calibration Results**
- Ice Accretion Results
- Summary
- Acknowledgements



### Introduction

- Development and use of 3D icing simulation tools.
- Lack of ice accretion and aerodynamic data for largescale, swept wing geometries.
- Aerodynamic understanding important for evaluating efficacy of 3D icing simulation tools.
- Multi-faceted research effort called SUNSET II.







## **Objective and Approach**

#### **Objective**

 Generate a database of ice-accretion geometry for large-scale, swept wings.

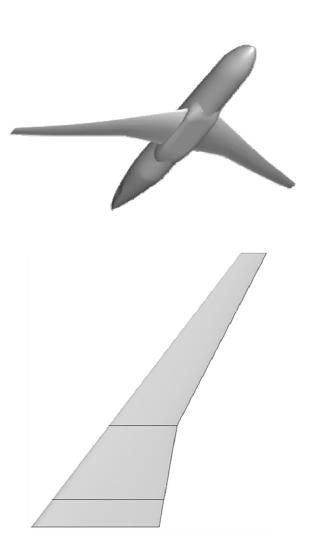
#### **Approach**

- Select baseline large-scale, swept-wing geometry.
- Identify three spanwise stations of interest—Inboard, Midspan and Outboard.
- Design hybrid or truncated wing-section models for IRT test section.
- Conduct ice-accretion testing in IRT.
- Measure ice geometry with 3D scanning technique.



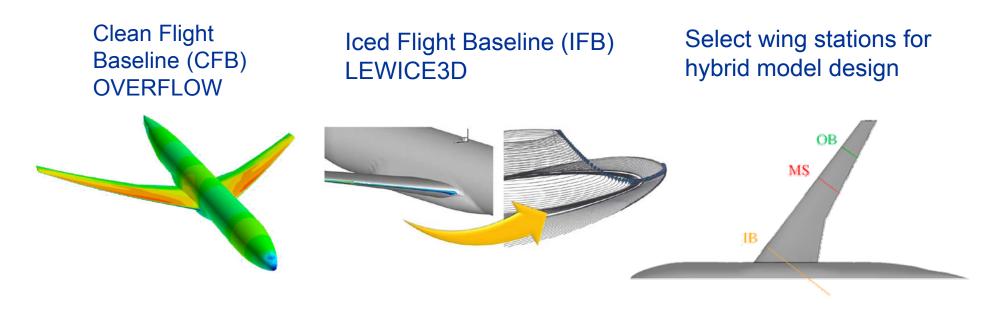
# **Common Research Model (CRM)**

- Commercial transport class configuration.
- Contemporary transonic supercritical wing design.
- Publically available and otherwise unrestricted for world-wide distribution.
- A 65% scale CRM was selected as the full-scale, reference swept-wing geometry for this research.
- CRM65 size airplane is comparable to Boeing 757.





## **Hybrid Model Design**



Design hybrid models to generate full-scale ice accretion.

Inboard, 20% Semispan	Midspan, 64% Semispan	Outboard, 83% Semispan
Scale Factor = 2.25	Scale Factor = 2	Scale Factor = 1.5



# **Experimental Methodology**

- Ice-accretion testing was conducted at NASA Icing Research Tunnel (IRT) that simulates flight through an icing cloud at pressure-altitudes near sea level.
- IRT test section is 6 ft high by 9 ft wide by 20 ft long.
- Models were installed vertically from floor-to-ceiling with small gaps to provide clearance for angle of attack and flap angle changes.

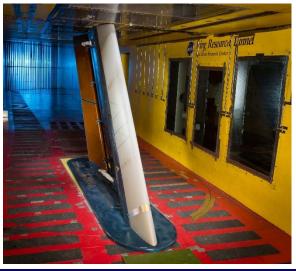
**Inboard Model** 



Midspan Model



**Outboard Model** 



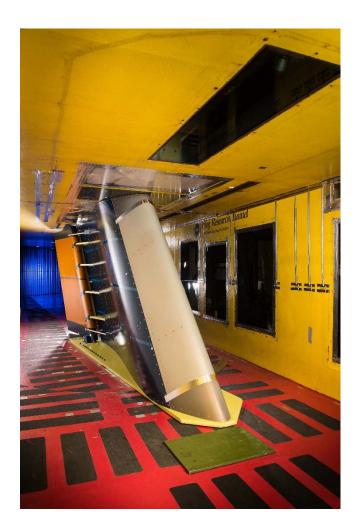


# **Experimental Methodology**

#### **Models Description**

- Streamwise pressure taps located at three spanwise stations
  - 18, 36 and 54 inches above the test-section floor.
- Single-element, slotted flap with antiicing heater.
- Two removable leading edges
  - Pressure instrumentation
  - Icing

Model Section	Streamwise Chord Length (ft)	Model Scale Factor
Inboard	13.5	2.25
Midspan	6.3	2.0
Outboard	6.2	1.5



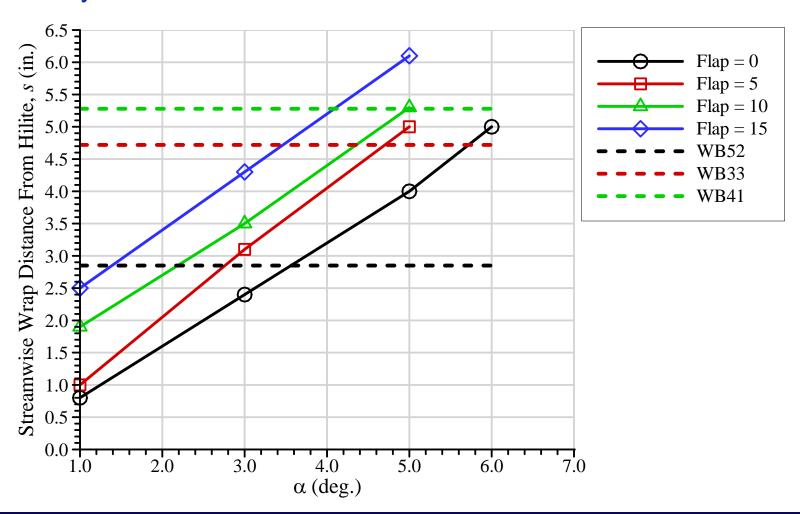


- An aerodynamic calibration of the hybrid models was performed in order to match the attachment point location on the IRT models to the corresponding location on the CRM65, full-scale reference airplane.
- The model incidence and flap angles were systematically varied to track the attachment line location at the 36-inch model centerline station.
- The attachment line location was defined as the location of the maximum pressure coefficient.

		Streamwise Wrap Distance—Inches From Hilite						
Flight Case	AoA deg.	Inboard Model	Midspan Model	Outboard Model				
WB33	3.7	4.72	1.66	1.06				
WB41	4.4	5.28	1.91	1.42				
WB52	2.1	2.85	0.57	0.36				

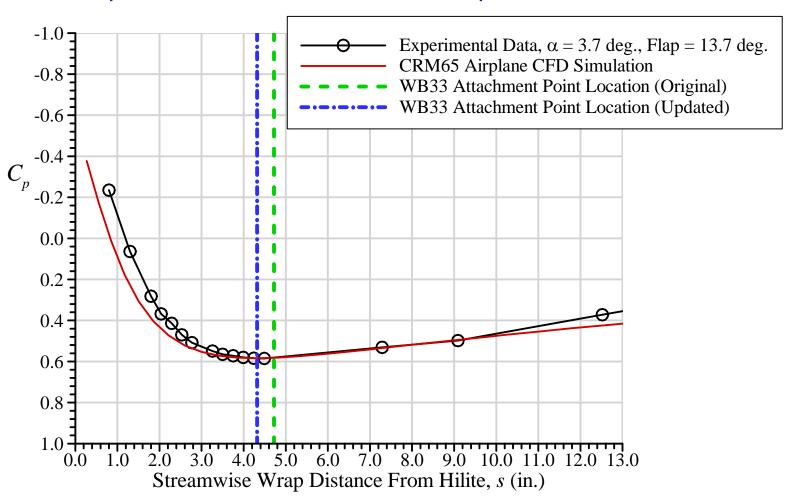


Aerodynamic calibration for Inboard Model.



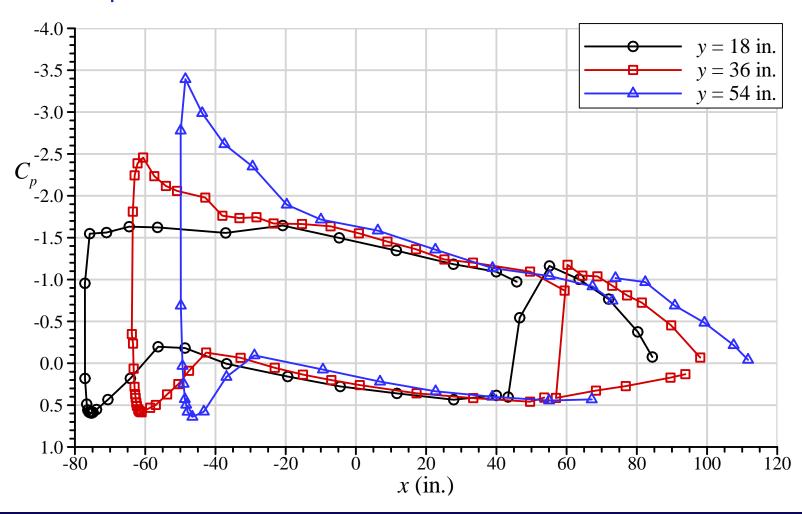


Surface pressure data near attachment point for Inboard Model.





Surface pressure data for Inboard Model.





### **Icing Test Matrix Development**

- Generate range of ice accretion.
- Hold and descent for CRM65 airplane in App. C.
- Large range of temperatures, limited variations in MVD and LWC.
- Large model size limited maximum speed in IRT.
  - Conditions were scaled to IRT test speed (130 knots for most cases).
  - Effects of velocity scaling were investigated for Midspan and Outboard models.

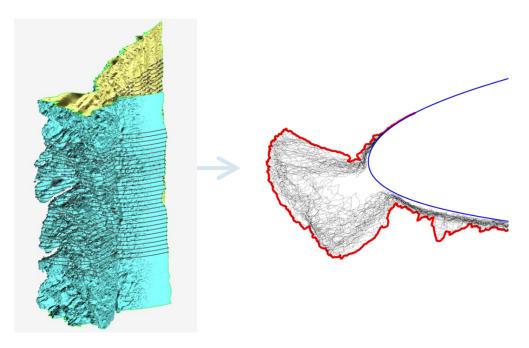
#### **Baseline Flight Reference Conditions**

Case	AoA deg.	Altitude (ft)	TAS Knots	Total Temp deg. C	Static Temp deg. C	MVD µm	LWC g/m <sup>3</sup>	Exp. Time min.
WB33	3.7	10,000	230	-18.4 to 1.1	-25.0 to -6.0	20	0.17 to 0.55	45
WB41	4.4	5,000	220	-6.0 to 1.1	-10.0 to -3.0	20	0.51	45
WB52	2.1	5,000	260	-4.1	-13.0	20	0.36	4



- Ice accretion was documented with photographs and 3D scans.
- 3D scan data were post-processed to provide the Maximum Combined Cross Section (MCCS).







Time lapse video—Midspan Model

Run	AoA deg.	TAS Knots	Total Temp deg. C	Static Temp deg. C	MVD µm	LWC g/m³	Exp. Time min.
TG2450	3.7	130	-6.3	-8.5	25	1.0	29





#### **Inboard Model—Effect of Temperature**

Run	AoA deg.	TAS Knots	Total Temp deg. C	Static Temp deg. C	MVD µm	LWC g/m <sup>3</sup>	Exp. Time min.
TG2421	3.7	130	-3.8	-6.0	25	1.0	29
TG2402	3.7	130	-8.7	-11.0	25	1.0	29
TG2415	3.7	130	-23.8	-25.0	25	1.0	29



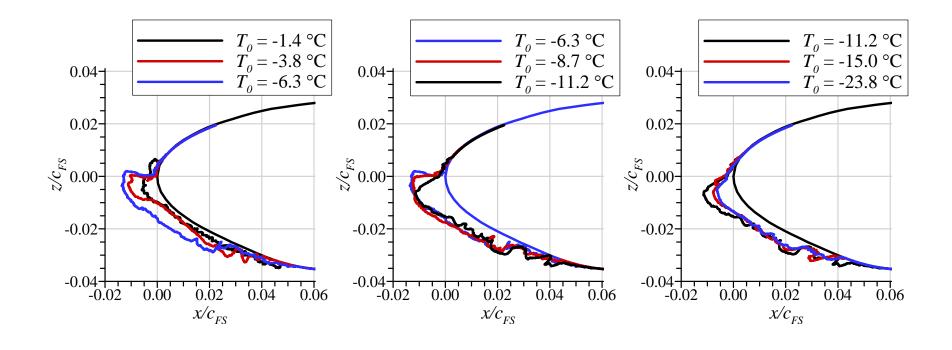






**Inboard Model—Effect of Temperature** 

Run	AoA deg.	TAS Knots	Total Temp deg. C	Static Temp deg. C	MVD µm	LWC g/m³	Exp. Time min.
-	3.7	130	-1.4 to -23.8	-3.6 to -25.0	25	1.0	29





Identical Condition Run on Each Model—Total Temperature = -3.8°C

Run	AoA deg.	TAS Knots	Total Temp deg. C	Static Temp deg. C	MVD µm	LWC g/m <sup>3</sup>	Exp. Time min.
TG2421	3.7	130	-3.8	-6.0	25	1.0	29
TH2438	3.7	130	-3.8	-6.0	25	1.0	29
TI2462	3.7	130	-3.8	-6.0	25	1.0	29



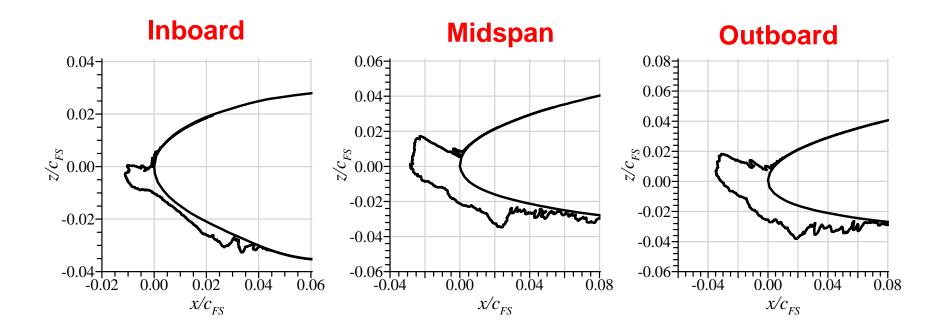






Identical Condition Run on Each Model—Total Temperature = -3.8°C

Run	AoA deg.	TAS Knots	Total Temp deg. C	Static Temp deg. C	MVD µm	LWC g/m <sup>3</sup>	Exp. Time min.		
TG2421	3.7	130	-3.8	-8.5	25	1.0	29		
TH2438	3.7	130	-3.8	-8.5	25	1.0	29		
TI2462	3.7	130	-3.8	-8.5	25	1.0	29		





Identical Condition Run on Each Model—Total Temperature = -6.3°C

Run	AoA deg.	TAS Knots	Total Temp deg. C	Static Temp deg. C	MVD µm	LWC g/m <sup>3</sup>	Exp. Time min.
TG2411	3.7	130	-6.3	-8.5	25	1.0	29
TH2452	3.7	130	-6.3	-8.5	25	1.0	29
TI2479	3.7	130	-6.3	-8.5	25	1.0	29



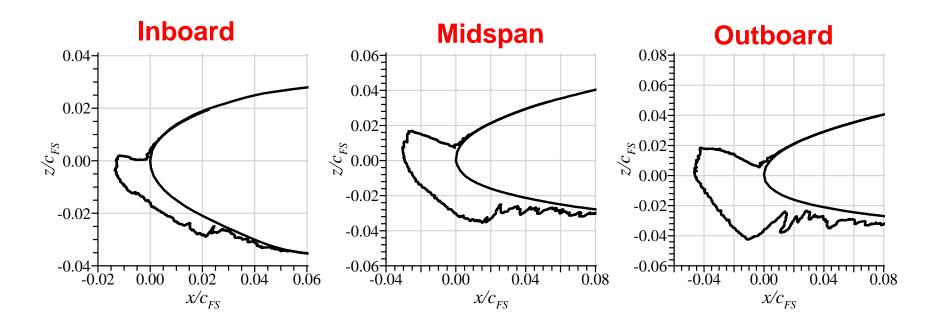






Identical Condition Run on Each Model—Total Temperature = -6.3°C

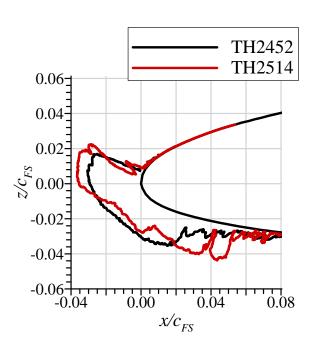
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Run	AoA deg.	TAS Knots	Total Temp deg. C	Static Temp deg. C	MVD µm	LWC g/m³	Exp. Time min.	
TG2411	3.7	130	-6.3	-8.5	25	1.0	29	
TH2452	3.7	130	-6.3	-8.5	25	1.0	29	
TI2479	3.7	130	-6.3	-8.5	25	1.0	29	





#### Maximum Scallop vs. App. C Scaled Conditions on Midspan Model

Run	AoA deg.	TAS Knots	Total Temp deg. C	Static Temp deg. C	MVD µm	LWC g/m <sup>3</sup>	Exp. Time min.
TH2452	3.7	130	-6.3	-8.5	25	1.0	29
TH2514	3.7	130	-3.1	-5.3	27	0.91	45



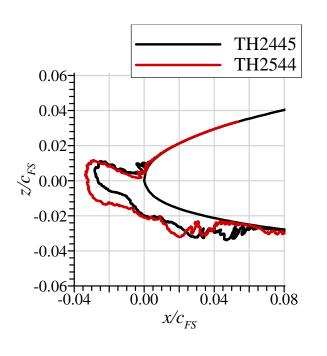






#### **Effect of Velocity on Ice Accretion on Midspan Model**

Run	AoA deg.	TAS Knots	Total Temp deg. C	Static Temp deg. C	MVD µm	LWC g/m <sup>3</sup>	Exp. Time min.
TH2445	3.7	130	-3.1	-5.3	27	0.91	32
TH2444	3.7	180	-2.0	-6.0	24	0.65	32



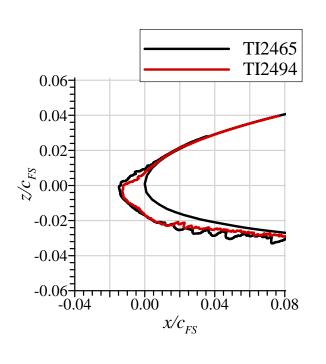






#### **Effect of Velocity on Ice Accretion on Outboard Model**

Run	AoA deg.	TAS Knots	Total Temp deg. C	Static Temp deg. C	MVD µm	LWC g/m <sup>3</sup>	Exp. Time min.
TI2465	3.7	130	-17.9	-20.1	25	0.60	23
TI2494	3.7	232	-11.2	-18.3	20	0.30	25.3









## **Summary**

- A large database of ice accretion geometry was generated for three sections of the CRM65 large-scale, swept wing.
- Hybrid models with full-scale leading-edges were used to obtain full-scale ice accretion at the Inboard (20%), Midspan (64%) and Outboard (83%) stations.
- The ice accretion database consists of the 3D ice accretion geometry along with surface pressure measurements on the clean hybrid models at corresponding aerodynamic conditions.
- For most cases, each model was subjected to identical icing conditions which limited the speed to 130 knots because of the large size of the Inboard model.
- The Appendix C-based icing conditions were scaled from flight reference values to account for the difference in velocity.
- A limited number of higher-velocity cases were run on the Midspan and Outboard models—results were limited by ice shedding.



## Acknowledgements

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#### **Supporting Organizations:**

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